

Problem 1

1.

$$P_{av} = [h / (\mu L)] [\exp (\mu L / h) - 1] \frac{2Y}{\sqrt{3}} \text{ where } h = (h_o + h_f) / 2 = 0.0625 \quad (1)$$

$$\Delta h = h_o - h_f = 0.025 \text{ so } L = \sqrt{R \Delta h} = \sqrt{4 (.025)} = 0.316, Y = 20,000 \quad (2)$$

Substituting, $P_{av} = [0.0625 / (0.1 \times 0.316)] [\exp (0.1 \times 0.316 / 0.0625) - 1] \times \frac{2 \times 20,000}{\sqrt{3}} P_{av} = 30,054 \text{ psi}$

2. Here we should use R' instead of R . We must calculate simultaneously F_s and R' .

Substituting $E' = 33 \times 10^6$, $R = 4$, and $\Delta h = 0.025$, in the equ. given in class for roll flattening gives:

$$\begin{aligned} F_s &= (R'/R - 1) \pi \Delta h E' / 16 \\ &= (R'/R - 1) \pi (0.025) (33 \times 10^6) / 16 \\ F_s &= 1.62 \times 10^5 (R'/4 - 1) \end{aligned} \quad (3)$$

and the equ. for the separating force becomes

$$F_s = (h/\mu) \left\{ \exp \left[(\mu/h) (R' \Delta h)^{\frac{1}{2}} \right] - 1 \right\} \times \frac{2 \times 20,000}{\sqrt{3}} \quad (4)$$

or

$$F_s = (0.0625/0.1) \left\{ \exp \left[(.1/0.0625) (0.025)^{\frac{1}{2}} \sqrt{R'} \right] - 1 \right\} \times \frac{2 \times 20,000}{\sqrt{3}} \quad (5)$$

or

$$F_s = 14,433 \left[\exp \left(0.253 \sqrt{R'} \right) - 1 \right] \quad (6)$$

Solving together equs. (3) and (6) gives the following:

$$R' = 4.24 \text{ and } F_s = 9,872 \text{ and } P_{av} = F_s / \sqrt{R' \Delta h} = 30,323 \text{ psi.}$$

3. Using the equ. given in class with $C = 7.5$,

$$h_{\min} = 7.5 (0.1) (4) \left(\frac{2 \times 20,000}{\sqrt{3}} \right) / (33 \times 10^6) = 0.0021 \text{ in} \quad (7)$$



2.11

Using the approximation for plane-strain compression with sticking friction, one can write:

$$P_{av} = 2\kappa \left(1 + \frac{b}{(4h)} \right) \text{ where } \kappa = \frac{Y}{\sqrt{3}} \quad (10)$$

and initially $b = h = 1$ and at the end of compression $b = 2, h = \frac{1}{2}$.

1. Substituting final values, $F = -20P_{av} = -20 \times 2 \left(\frac{2500}{\sqrt{3}} \right) \left[1 + \frac{2}{4 \times .5} \right] = -115,500$ pounds (the minus sign for compression).

2.

$$\begin{aligned} W &= \int F dh; \text{ substituting } F = -P_{av} \times 10b \text{ and } P_{av} = 2\kappa [1 + b/(4h)] \\ W &= \int F dh = -2\kappa \int [10b [1 + b/(4h)]] dh, \text{ but } b = 1/h \text{ (since } bh = 1) \text{ so} \\ W &= -2\kappa \int [10(1/h) [1 + (1/h)/(4h)]] dh = -20\kappa \int [1/h + (1/(4h^3))] dh = \\ &= -20\kappa \left[\ln(h_f/h_o) + (-1/8)(h_f^{-2} - h_o^{-2}) \right] \end{aligned} \quad (11)$$

Evaluating at $h_o = 1$ and $h_f = \frac{1}{2}$,

$$\begin{aligned} W &= -20\kappa \left[\ln\left(\frac{1}{2}\right) - \frac{1}{8}(4 - 1) \right] = -20\kappa \left[\ln\left(\frac{1}{2}\right) - \frac{3}{8} \right] = -20\kappa (-1.068) \\ &= 20 \left(\frac{2500}{\sqrt{3}} \right) (1.068) = 30,800 \text{ in} - \text{lbs. (2,570 ft} - \text{pounds)} \end{aligned}$$

3. Ideal work, $W_i = \text{volume} \cdot Y\bar{\epsilon} = 10 \text{ in.}^3 \cdot 2,500 \text{ psi} \cdot \frac{2}{\sqrt{3}} \cdot \ln(2) = 20,000 \text{ in} - \text{lbs}$

$$\eta = \frac{W_i}{W_a} = 20,000 \text{ in} - \text{lbs} / 30,800 \text{ in} - \text{lbs} = 65\%.$$

113.

$$a) \quad h_{min} = \frac{7.5 \times 0.3 \times 5}{\frac{30 \times 10^6}{1 - 0.33^2}} \left(\frac{2}{\sqrt{3}} 31,000 \right)$$

$$\boxed{h_{min} = 0.012 \text{ in}}$$

b) CONSERVATION OF VOLUME

$$h_{min} \underbrace{V_*}_{\text{EXIT VELOCITY}} = 0.02 \times 37 \times 12 \text{ IN}^3/\text{s}$$

0.012 IN EXIT VELOCITY

$$\boxed{V_* = 740 \text{ IN}^3/\text{s} = 61.7 \text{ ft}^3/\text{s}}$$

$$c) \quad P_{AUG} = \frac{h}{\mu L} \left(e^{\frac{\mu L}{h}} - 1 \right) \frac{2Y}{\sqrt{3}}$$

$$= \frac{\frac{0.02 + 0.012}{2}}{0.3 \sqrt{5(0.02 - 0.012)}} \left(e^{\frac{0.3 \sqrt{5(0.02 - 0.012)}}{\frac{0.02 + 0.012}{2}}} - 1 \right) \frac{2 \times}{\sqrt{3}} (31,000)$$

$$P_{AUG} = \frac{0.016}{0.06} \left(e^{\frac{0.06}{0.016}} - 1 \right) (35,796)$$

$$= 396,349 \text{ PSI}$$

$$F = P_{AUG} L W$$

$$= (396,349) \sqrt{5(0.02 - 0.012)} (13)$$

$$\boxed{F = 1.03 \times 10^6 \text{ LBF}}$$

d) SEE CLASS NOTES

4.
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$$P_{AVG} = Y + \frac{2KR}{3h}$$

$$K = \frac{Y}{\sqrt{3}}$$

$$P_{AVG} = Y + \frac{2YR}{3\sqrt{3}h}$$

$$= 25,000 + \frac{2(25,000)(0.95)}{3\sqrt{3}(0.06)}$$

$$= 101,178 \text{ PSI}$$

$$F = P_{AVG} \cdot \pi R^2$$

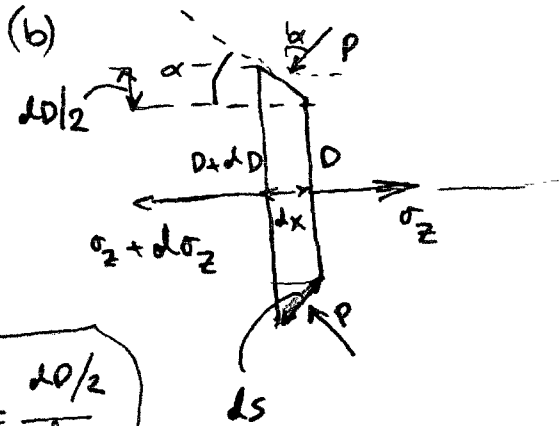
$$\underline{\underline{F = 71,717 \text{ LBF}}}$$

5. (a) $\left\{ \begin{array}{l} \sigma_r = \sigma_\theta \text{ (axisymmetric assumption)} \\ \sigma_z \end{array} \right.$

$$\bar{\sigma} = Y \Rightarrow \frac{1}{\sqrt{2}} \sqrt{(\sigma_r - \sigma_\theta)^2 + (\sigma_\theta - \sigma_z)^2 + (\sigma_z - \sigma_r)^2} = Y \Rightarrow$$

$\sigma_r = -P \qquad \sigma_z = -P$

$$\frac{1}{\sqrt{2}} \sqrt{(\sigma_z + P)^2 + (\sigma_z + P)^2} = Y \Rightarrow \boxed{\sigma_z + P = Y}$$



$$\sum F_z = 0 \rightarrow$$

$$(\sigma_z + d\sigma_z) \frac{\pi}{4} (D + dD)^2 - \sigma_z \frac{\pi}{4} D^2$$

$$+ p \sin \alpha (\pi D ds) = 0$$

attention with the area

NO FRICTION
HERE

(Compare with
Problem 7/HW10)

$$\Rightarrow \frac{\pi}{4} d\sigma_z D^2 +$$

$$\cancel{\sigma_z \frac{\pi}{4} (dD)^2} \quad \text{2nd order}$$

$$+ \cancel{d\sigma_z \frac{\pi}{4} 2D dD} + \cancel{\sigma_z \frac{\pi}{4} 2D dD} + p \sin \alpha \pi D \left(\frac{dD}{2} \frac{1}{\sin \alpha} \right) = 0$$

$$\Rightarrow \frac{\pi}{4} d\sigma_z D^2 + \sigma_z \frac{\pi}{4} 2D dD + p \pi \frac{D}{2} dD = 0 \rightsquigarrow$$

$$D d\sigma_z + 2\sigma_z dD + 2p dD = 0 \Rightarrow$$

Substitute from (a) $\sigma_z = -P + Y \Rightarrow$

$$-D dp + 2(-P + Y) dD + 2P dD = 0 \Rightarrow$$

$$D dp = + 2Y dD \Rightarrow \boxed{\frac{dP}{2Y} = \frac{dD}{D}}$$

(c)

$$\int_Y^P \frac{dP}{2Y} = \int_{D_0}^D \frac{dD}{D}$$

note at $D = D_0$, $\sigma_x = 0 \Rightarrow \cancel{\sigma_x} + P = Y \Rightarrow$
 $P|_{D=D_0} = Y$

$$\Rightarrow \frac{1}{2Y} (P - Y) = -\ln \frac{D_0}{D} \Rightarrow$$

$$P = Y - Y \ln \left(\frac{D_0}{D} \right)^2 \rightarrow \boxed{P = Y \left[1 - \ln \left(\frac{D_0}{D} \right)^2 \right]}$$

116.

$$W_a = W_c + W_s + W_r$$

$$W_s = 0.4 W_c$$

$$W_r = 0.25 W_a$$

$$\Rightarrow 0.75 W_a = 1.4 W_c$$

$$\frac{W_c}{W_a} = \eta = \frac{0.75}{1.4} = 0.536$$

$$P_e = \frac{\int_0^{\epsilon_s} \bar{T} d\bar{\epsilon}}{\eta} = \frac{k \epsilon_a^{n+1}}{(n+1)\eta}$$

$$\epsilon_a = 2 \ln \left(\frac{D_o}{D_s} \right)$$

$$= 2 \ln \left(\frac{6}{2} \right)$$

$$= 2.2$$

$$P_e = \frac{(26,000)(2.2)^{1.2}}{1.2(0.536)} = 104,120 \text{ PSI}$$

$$F_e = P_e \left(\frac{\pi D_o^2}{4} \right)$$

$$F_e = 2.94 \times 10^6 \text{ LBF}$$
